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AMENDMENTS TO THE DRAWINGS

Please replace the original drawing sheets for figure 1 bis and figure 5 with the enclosed replacement sheets.

REMARKS

This Amendment is fully responsive to the non-final Office Action dated January 10, 2008, issued in connection with the above-identified application. Claims 1-10 were previously pending in the application. With this Amendment, claims 1 and 3-10 have been amended; claim 2 has been canceled without prejudice or disclaimer to the subject matter therein; and claim 11 has been added. Accordingly, claims 1 and 3-11 are now all the claims currently pending in the application. No new matter has been introduced by the amendments made to the claims or by the new claim added.

At the outset, the Applicants' thank Examiner Davis for granting the interview conducted with the Applicants' representative on April 2, 2008. During the interview, the present invention as described in previous claim 1, and the Furuya reference were discussed in detail. It was also suggested that claim 1 be amended to point out that the second supply channel includes a differential pressure measuring device that is operable to detect and measure the presence or absence of a gas flow passing through the second supply channel at a pre-determined time after a blow-moulding phase has started. Additionally, it was noted that Furuya fails to disclose or suggest the use of a differential pressure measuring device as recited in claim 1 (as now amended).

At the conclusion of the interview, it was agreed that the Furuya reference discloses some type of pressure detecting device, but it is not clear from the reference whether the detecting device is a differential pressure measuring device or if the detecting device is configured as suggested in claim 1. Accordingly, the Examiner indicated that the proposed claim amendments to claim 1 would likely distinguish the claim from Furuya. However, the Examiner also indicated that further search and consideration would be necessary before making a final determination regarding the allowability of the claims.

To facilitate the Examiner's reconsideration of the application, the Applicants have provided a substitute specification and abstract. The changes to the specification and abstract include minor editorial and clarifying changes. In addition to the substitute specification and abstract, a marked-up copy of the original specification and abstract are also enclosed. No new

matter has been added by the changes made to the specification and abstract.

The Applicants have also made various amendments to the claims to place the claims in better form for U.S. patent practice. These amendments were not made to address any prior art rejections noted by the Examiner (e.g., under 35 U.S.C. 103). The only amendments made to address the prior art rejections by the Examiner are noted below in the discussion of the prior art rejections.

In the Office Action, the Examiner objected to the drawings and the specification based on minor informalities. Specifically, the Examiner noted that Fig. 5 includes reference numerals 3 and 4 to refer to ports 53 and 54 (i.e., as described on line 24, page 13 of the specification). Additionally, the Examiner noted that Fig. 6A does not have a brief description in the specification. Accordingly, the Applicants have provided herein a replacement sheet for Fig. 5 that corrects the labeling of the ports noted by the Examiner. Also, the Applicants have amended the specification to include a brief description for Fig. 6A. Withdrawal of the objections to the drawings and the specification is respectfully requested. The Applicants have also provided a replacement sheet for Fig. 1bis to change the number of the figure to Fig. 1A.

In the Office Action, claims 1 and 2 have been rejected under 35 USC 103 as being unpatentable over Weiss (U.S. Patent No. 5,648,026, hereafter "Weiss") in view of Furuya et al. (Japanese Patent No. 4-298322, hereafter "Furuya"). The Applicants have canceled claim 2 rendering the above rejection to that claim moot. Additionally, the Applicants have amended independent claim 1 to be consistent with the claim amendments discussed during the examiner interview conducted on April 2, 2008. Thus, claim 1 (as now amended) should be clearly distinguished from the cited prior art.

As amended, claim 1 recites the following features:

"A blow moulding apparatus for producing hollow bodies of plastic material obtained from respective preforms, comprising:

at least one blow-moulding die configured to contain a plurality of cavities, each cavity being configured for blow moulding respective preforms,

a main conduit operable to supply gas into the plurality of cavities provided inside the

blow-moulding die,

a low-pressure gas supply source connected to said main conduit via a first supply channel,

- a first controlled valve provided to the first supply channel,
- a high-pressure gas supply source connected to said main conduit via a second supply channel,

a second controlled valve provided to the second supply channel,

wherein the second supply channel includes a differential pressure measuring device operable to detect and measure a presence or an absence of a gas flow passing through the second supply channel at a pre-determined time after a blow-moulding phase has started." (Emphasis added).

At least the features emphasized above are not believed to be disclosed or suggested by the cited prior art. Additionally, the features emphasized above are fully supported by the Applicants' disclosure (see e.g., Fig. 1A (formally Fig. 1bis)).

As amended, claim 1 more particularly points out that the second supply channel includes a differential pressure measuring device that measures the gas flow in the second supply channel. The second supply channel is responsible for the final blowing stage of the moulding process in which the volume and shape of the container being moulded is kept almost constant by a high pressure. Thus, the use of the differential pressure measuring device in the second supply channel provides detection of the container's condition and helps to reduce the possibility of the container rupturing or exploding during the final blowing stage. As noted during the examiner interview, the cited prior art fails to disclose or suggest at least the use of a differential pressure measuring device as described in claim 1.

In the Office Action, the Examiner relied exclusively on Furuya for disclosing or suggesting the use of a pressure detection device that measures the presence or absence of a gas flow passing through a supply channel during a blow-moulding operation. Specifically, the Examiner noted that Weiss "does not disclose a means for measuring the presence of absence of a gas flow through a channel" (see e.g., Office Action, page 3). Accordingly, the Examiner relied

exclusively on the abstract and Figs. 1-6 of Furuya for disclosing or suggesting this feature.

More specifically, the Examiner relied on the pressure detector 11 disclosed in Furuya for disclosing or suggesting the pressure measuring device of claim 1. However, as amended, claim 1 specifically recites a <u>differential pressure measuring device operable to detect and measure the presence or absence of a gas flow passing through the second supply channel at a pre-determined time after a blow-moulding phase has started.</u>

On the other hand, the abstract of Furuya discloses an apparatus for detecting a faulty state of an item being moulded during blow moulding. As described, a faulty state of the item is detected without removing the item from the mould by comparing blow pressure, suction pressure, and sound output with information at a normal state. However, the abstract of Furuya fails to even mention the pressure detector 11.

Additionally, although Figs. 1-6 of Furuya disclose the pressure measuring detector 11, Figs. 1-6 also fail to give any hint that the detector 11 is a <u>differential pressure measuring device</u>, let alone a differential pressure device that is operable to detect and measure the presence or <u>absence of a gas flow passing through the second supply channel at a pre-determined time after a blow-moulding phase has started</u>, as recited in claim 1.

Based on the above discussion, claim 1 is clearly not anticipated or rendered obvious by the cited prior art.

In the Office Action, claims 3-10 have been rejected under 35 U.S.C. 103(a) as being unpatentable over Weiss in view of Furuya, and further in view of Cutler (U.S. Patent No. 4,592,239, hereafter "Cutler").

Claims 3-10 depend from independent claim 1. As noted above, Weiss and Furuya fail to disclose or suggest all the features recited in claim 1 (as amended), individually or in combination. Additionally, Cutler fails to overcome the deficiencies noted above in Weiss and Furuya. That is, Cutler fails to disclose or suggest a <u>differential pressure measuring device</u>, let alone a differential pressure device that is operable to detect and measure the presence or absence of a gas flow passing through the second supply channel at a pre-determined time after a blow-moulding phase has started, as recited in claim 1.

Accordingly, no combination of Weiss, Furuya and Cutler would result in, or otherwise render obvious, claims 3-10 based at least on their dependency from independent claim 1.

Moreover, new dependent claim 11 is not believed to be anticipated or rendered obvious by the cited prior art for the same reasons noted above for claims 1 and 3-10.

In light of the above, the Applicants respectfully submit that all the pending claims are patentable over the prior art of record. The Applicants respectfully request that the Examiner withdraw the rejections presented in the Office Action dated January 10, 2008, and pass this application to issue. The Examiner is also invited to contact the undersigned attorney by telephone to resolve any remaining issues.

Respectfully submitted,

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Version with Markings to Show Changes Made

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10 APPARATUS AND METHOD WITH SPECIFICALLY PROVIDED DEVICE FOR AUTOMATIC BURST DETECTION IN BLOWMOULDED CONTAINERS

DESCRIPTION

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Background of the Invention

The present invention refers to an apparatus and a method for the production of hollow plastic articles, or plastic containers, in particular bottles, in which use is made of a specifically provided device adapted to identify bottles that have possibly been blow-moulded in a faulty manner and must therefore be rejected.

Although reference will be made in the following description, mainly for reasons of greater descriptive convenience, to an apparatus for blow moulding bottles of plastic material, it will be appreciated that the present invention shall be understood as applying also to other kinds of plants and processes, as far as these fall within the scope of the appended claims.

Largely known in the art are plants and methods for blow moulding plastic bottles that are obtained by filling with gas under pressure

appropriately heated plastic semi-processed elements, which are generally known by their technical name of "parisons" or "preforms" in the art.

Plants of such a kind are for instance described in the European patent application no. 96114227.0 of this same Applicant, as well as in the various patent publications cited therein.

It is rather largely known in the art that, during the preform blow-moulding process, the possibility is quite often given that that, (owing to a number of most varied reasons, which on the other hand shall not be discussed here owing to them not having any relevance to the present invention invention,) some production irregularities or disturbances may occur to such an extent as to cause some preforms, in a random sequence thereof, to expand in an incorrect manner. Additionally, some preforms are manner, although blow-moulded regularly, up to the point that they may even burst either before reaching their final shape or immediately thereafter, while they still dwell inside the blow-moulding die.

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Furthermore, the possibility also arises that the same preforms turn out to be already cracked and/or defective even before that the actual blow-moulding process takes place, so that it is practically impossible for the same preforms to be blown, even partially, to the final shape thereof.

When such an event occurs, the blow-moulding plant goes on operating, but even when the bottles that have so burst. Therefore, some bottles that fail and, therefore, failed to be completed correctly continue to be transported transported, although in their form of fully useless rejects, on the subsequently provided conveyance line together with the correctly produced bottles. and, again Additionally, together with saidthe correctly produced bottles, they are eventually collected in appropriate storage bins or similar containers before being sent to final utilization.

As far as this particular step is concerned, the need therefore arises for either manual or mechanical and partly automated means to be provided

to-identify possible faulty bottles and remove them from the conveying, collecting and storage means as described above.

Such an operation does of course not fail to generate corresponding production costs and charges, which are quite frequently fully unacceptable in an industrial environment that is subject to a high extent of pressure in terms of manufacturing competition. It anyway introduces a complication in the manufacturing process, since it necessarily implies an addition of auxiliary operations that must be carried out by appropriate operators, usually on an off-line basis.

In an attempt to find a remedy for such a situation, the patent application PCT/EP 01/01571, filed by this same Applicant with the title "BLOW-MOULDING PLANT WITH APPARATUS FOR AUTOMATIC BURST DETECTION IN BLOW-MOULDED CONTAINERS", describes an apparatus and a method for identifying bottles which have failed, i.e. burst during the blow-moulding process.

For greater convenience, simplicity and brevity in this description, direct reference should therefore be made to such a document for a better insight in the disclosure thereof.

Briefly, anyway, such athe above document discloses a blow-moulding apparatus that comprises, further to the usual elements and components, a specially provided acoustical/electric transducer arrangement adapted to detect the noise issued outside by the individual moulds. And, the acoustical/electric transducer arrangement converts moulds, and convert such a noise into an electric signal. Additionally, signal; there are provided means that process this signal and compare it with a reference signal; provide provided are also means that, on the basis of the result of such a comparison, identify identifies burst or failed containers, as well as means that are adapted to automatically and selectively exclude the exclude said-burst or failed containers from the production line.

The apparatus described in the above-mentioned patent application has turned out as being actually capable of being implemented without any practical difficulty at all, as well as quite effective in blow-moulding bottles. However, practical experience on the production floor has caused some drawbacks (as noted below) to come to light, which for the matter are still being experienced with such a kind of apparatus. apparatus:

-aA first drawback lies actually in the marked noisiness of the whole plant. As plant; as a matter of fact, these plants, especially when they are single-stage plants and, above all, when they are installed in an environment that includes other noisy industrial plants, are subject to a continuous, high-intensity acoustic stress from both the noise falling upon them from the outside and the noise that they generate themselves.

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It has been found that, unacceptably too often, such a high noise level, which these plants are exposed to, can disguise the noise generated by a bursting preform (owing to the need for the intensity of the reference signal to be increased correspondingly), so that it fails to be detected and, as a result, the resulting defective product fails to be promptly removed from the production line, thereby making the detection arrangement of the described invention partially ineffective.ineffective;

—aA second drawback is connected with the circumstance that the preform that reaches the blow-moulding station for being blown into the final product, is itself defective or damaged, thereby showing cracks that, however small they may also be, prevent the same preform from being blown into its final bottle shape due to the blowing gas leaking therethrough.

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In this case, i.e. in the event of such failed blow-moulding operations due to already existing leaks in the preform, not even the typical noise generated by a bursting preform is actually generated, so that it is not possible for either the presence of a production reject to be identified or, even less, the same production reject to be removed from the regular production flow.

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In view of trying to find a remedy for these problems through the use of means for the detection of the pressure differences occurring whenever a preform being blow-moulded bursts, or in the event of a cracked preform failing to be blow-moulded, the solution has been considered of using suitable pressure detectors adapted to measure the pressure of the gas in 10 the flow path followed by it when flowing into the container being blowmoulded. It has however been found that, when the bottles are being blow-moulded individually in a sequence, the pressure detector arrangement to be used must in that case be capable of withstanding very high pressures, up to approximately 40 bar, and at the same time measuring abrupt and marked pressure drops.

This is actually achievable with the use of industrial component parts that are currently available on the market; however, if the preforms, instead of bursting when being blown, are defective, i.e. cracked since the 20 beginning, the reduction in pressure that takes place in this case may be so small as to fail to be either detected at all, or detected regularly and unfailingly each time, by a pressure detector arrangement that has been provided in view of being capable of operating at far higher pressures or detecting total pressure drops. On the contrary, in the most usual and 25 common case that a plurality of preforms are blow-moulded simultaneously from a single source supplying gas under pressure (i.e. the so-called in-line blow-moulding process), the pressure detector arrangement to be used must be capable of withstanding modest pressure variations taking place very rapidly. Further rapidly; further to the difficulty encountered in finding out such a suitable type of pressure detectors, the need also arises in this case for the fact to be considered that a pressure variation as measured in the gas supply conduit can be indicative of a blow-moulding die operating in an irregular manner, but fails to identify which mould is actually concerned.

Summary of the Invention

It therefore is desirable, and it is actually a main object of the present invention, to provide an apparatus and a respective method that are capable of performing an automatic preform blow-moulding process and, at the same time, are provided with means that are capable of identifying in a substantially immediate manner those dies in which a preform is possibly blown to bursting, and keeping track of any so resulting reject so as to be able to put apart, in a fully automatic manner at an appropriate station through which saidthe faulty preforms are due to pass, all such faultily blow-moulded preforms in the state of rejects.

In addition, saidthe means must be capable of working without any limitation at all in a highly noisy environment and, at the same time, must also be capable of identifying those failed blow-moulding operations that substantially occur without generating any particular noise signals, such as in the case of already cracked preforms.

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Such an apparatus and related method shall furthermore be reliable, fully efficient and operatively effective, as well as capable of being implemented through the use of readily available techniques and materials.

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According to the present invention, these and further aims are reached in an apparatus and a method that are made and operate with the characteristics as recited in the appended claims.

Brief Description of the Drawings

The present invention may be implemented in the form of a preferred embodiment that is described and illustrated in detail below by way of non-limiting example with reference to the accompanying drawings, in which:

- Figure 1 is a purely schematic view of an apparatus according to the present invention;

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- Figure 1BISA is an enlarged, symbolical view of a section of the apparatus shown in Figure 1;

- Figure 2 is a diagrammatical view of the course of the internal 10 pressure in a bottle during a regularly performed and occurring blow-moulding operation;

- Figure 3 is a diagrammatical view of a typical course of the differential pressure as detected during a blow-moulding operation in an apparatus of
 the kind illustrated in Figure 1, with a positive result of the same blow-moulding operation;
 - Figure 4 is a diagrammatical view of the course of the differential pressure as detected during and after a blow-moulding operation in a same apparatus, in which the bottle being blown has burst;
 - Figure 5 is a view of a first variant of the apparatus shown in Figure 1;
- 25 Figure 6 is a view of a second improved variant of the apparatus shown in Figure 1;
 - Figure 6A is a view of third improved variant of the apparatus shown in Figure 1;

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- Figures 7 and 8 are diagrammatical views of the course of the differential pressure in the case of faulty preforms, in a situation similar to the one considered in Figure 4, but with an expanded pressure scale.

Detailed Description of the Invention

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The present invention is essentially based on the observation that when, during the blow moulding of a preform, the latter undergoes tearing or breakage, one of the most immediate consequences of such an occurrence is a clearly perceptible and detectable explosion. that That is due to the fact that the compressed air inside the preform being so blow-moulded escapes abruptly and violently through the leak so formed in the wall of said-the preform and causes a corresponding variation in the flow of air or gas being supplied into the preform itself to blow it into its final shape.

In order to more effectively describe this particular occurrence, reference is made to the illustration in Figure 2, which shows a diagram that has been plotted of the actual course of the pressure inside a preform being blown, or in the conduit of the air being supplied to such a purpose, during a blow-moulding operation performed and taking place in a regular and correct manner. There may be identified four main phases, wherein phase A refers to the preform being filled with gas supplied at low pressure, while almost simultaneously undergoing a stretching action that may take place either just before or just after saidthe low-pressure gas supply is started. This phase therefore implies a significant flow of gas, and the perform is caused to blow up and expand into almost reaching the final shape of the bottle to be produced, while the pressure remains however at a low level.

In the following phase B, gas is let in at a quite high pressure, typically at approximately 40 bar, owing to the fact that the bottle, which at this point is almost moulded to its final shape, must be pressed against the blow-moulding die in view of being able to take its definitive, detailed shape.

Since this phase is carried out at an almost constant volume, the pressure inside the bottle builds up rapidly to reach its almost maximum value, while the flow decreases to the point it reaches almost zero.

In the next phase C, the high pressure inside the bottle is kept for a time as deemed necessary in view of enabling the bottle to stabilize and consolidate its definitive shape. The pressure is kept at its maximum value, while the gas inflow is practically zero (in the assumption that there are no leakages). In the final fourth phase D, the gas contained in the bottle is released therefrom, so that its pressure decreases rapidly to zero (atmospheric value).

It has been observed that, when a bottle turns out to be perforated, cracked or burst, at the end of the phase B and throughout the following phase C, inside the pipe that carries the air at 40 bar there is a substantial flow of gas, and it is actually this flow of gas that has desirably to be measured, since it is the most effective indicator of the existing air or gas leakage.

It has in fact been found that, if the bottle is not perforated, cracked or burst, such a flow of air tends to end up just after a very short time that the high-pressure air valve is opened.

If the bottle is on the contrary perforated, cracked or burst, or anyway there is a leakage indicative of an irregular blow-moulding operation, the high-pressure air flow keeps going on at a certain value, which is certainly detectable and may sometimes be also quite elevated, well beyond the duration of the phase C.

For the magnitude of the flow inside the supply conduit to be able to be determined in an accurate and reproducible manner, the need arises for a device and a related method to be provided, which do not alter pressure losses to any significant extent, are capable of withstanding static

pressures of up to approximately 40 bar, and are resistant to the conditions imposed by working cycles that follow each other uninterruptedly within the conduit under turbulent flow conditions.

- An apparatus provided with the device according to the present invention is comprised of following component parts (see Figure 1):
 - a plurality of dies 100 for blow-moulding preforms,

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- a main conduit 1 that carries the air into the cavities of the blow-moulding dies,
 - a low-pressure gas supply source 103 connected to saidthe main conduit 1 via a respective first supply channel 101,
 - a suitably controlled valve 102 associated to saidthe first supply channel,
- a high-pressure gas supply source 104 connected to saidthe main conduit 1 via a respective second supply channel 105,
 - a second suitably controlled valve 106 associated to saidthe second supply channel.
- In this example of embodiment, the invention consists inincludes providing saidthe second supply channel 105 with a particular embodiment of a Pitot tube arrangement (which is widely known in the art, so that it shall not be described here any further). It is a largely known fact that such a device is capable of detecting and measuring even very low flow speeds: when a gas flows through the Pitot tube at a certain speed V, a pressure difference builds up across the tubes, on which this Pitot tube arrangement is based, such a pressure difference being proportional to the square of the speeds of the flow.

In this particular case, two small tubes 3, 4 are inserted in saidthe supply channel 105, where they are arranged so as to extend across saidthe channel orthogonally thereto. These tubes must be given as small a size as possible, so as to avoid adding any significant disturbance of the flow to be measured; they must anyway be given a properly calibrated cross-section.

Both these small tubes have a respective bore 5, 6 extending along an axis aligned with the direction of the flow, but oriented in an opposite direction with respect to each other, i.e. the projection of a first bore 5 on a plane orthogonal to the direction of the flow, downstream of the same bore, is not nil, whereas nil is the projection thereof on the plane orthogonal to the direction of the flow, but upstream of the bore.

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Exactly the opposite is true as far as the second bore 6 is concerned, as this is illustrated in Figure 1Bis.A.

Arranged in each one of saidthe two small tubes there is a suitable pressure sensor 7 and 8, respectively, wherein saidthe sensors are connected to a same differential pressure detector arrangement 10.

With the apparatus configured as defined and described above, a number of experiments have been carried out in order to identify the typical course of the differential pressure and, accordingly, of the speed of the flow of blowing gas, in the two opposite conditions of:

- regular blow-moulding with positive result (no leakage) and
- or perforation.

Figure 3 shows in a general manner a typical course of the differential pressure detected during blow moulding in a 16-cavity die, without any

bottle bursting or breaking, whereas Figure 4 shows a typical course of the differential pressure as detected during and after a blow-moulding operation in a same apparatus, in which the bottle being blown has burst.

It clearly emerges from the illustration in Figure 3 that the differential pressure plotted on the ordinate, and therefore the flow, increases from an initial value of zero up to a maximum value, and then decreases again to saidthe initial value of zero at the end of the blow-moulding process, and this can only be taken as an indication of a successfully blown bottle, since it is only in this case that the flow decreases progressively to zero during the total filling cycle.

In the opposite case, i.e. when a bottle bursts during blow moulding, as this is best illustrated in Figure 4, the differential pressure, and hence the flow, increases from an initial value of zero up to a maximum value P_M, and then decreases again to a value that anyway is higher than zero, i.e. P_S > 0, and this can only be taken as an indication of a bottle having burst during blow moulding, or anyway leaking, since it is only in this case that the flow may well decrease during high-pressure gas blowing, but will never reach down to zero.

Owing to the rather small-scale representation in Figure 4, in order to be able to take a closer look at and more accurately follow the course of the pressure as detected in some similar cases, in which the bottles have burst during blow moulding, some experiments have been reproduced.

The reproduced, the results of which the experiments are illustrated in Figures 7 and 8, in which the vertical or pressure scale is expanded. In particular, Figure 7 indicates the course of the typical ΔP of a bottle that, while not burst, is punctured, whereas Figure 8 indicates the typical ΔP of a bottle that has burst.

Going on with the investigation of such phenomena, it has been most clearly observed that, in each one of the cases represented in the above cited Figures, it is possible to identify a positive (i.e. higher than zero) average differential pressure, which is assumed as being the reference differential pressure P1, associated to and persisting over a certain definite period of time T1 after the beginning of the blowing phase; defined is then most suitably also a maximum threshold value P2 of the differential pressure, to which conventionally corresponds a decision whether there is a leakage during blow moulding or not.

When the differential pressure being measured at that definite moment, or even during a pre-established period of time, exceeds said the pre-established maximum threshold value of differential pressure P2, it can then be concluded with a reasonable level of confidence that the blow-moulding operation has failed to be completed successfully due to the existence of more or less marked gas leakages or losses.

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Going back at this point to Figure 1BisA, the differential pressure detector arrangement 10 is connected to an appropriate processing means 11, which is capable of receiving the signals coming from saidthe differential pressure detector arrangement 10, measuring the value thereof, receiving and storing reference levels set by the external operator, comparing saidthe values with saidthe reference levels and, based on the outcome of such a comparison, generating appropriate command and control signals to be sent to further actuation means (not shown), which are made and arranged in an appropriate manner so as to be able to exclude, i.e. remove from the production process those bottles which are told to be defective by the outcome of saidthe comparison.

These operations and means for processing electric and electronic signals, as well as comparing and producing control and actuation signals are fully and readily available to and within the capability of all those skilled in the art of industrial automation, so that they shall not be described in any greater detail here.

The described invention may furthermore be embodied so as to include following advantageous improvements: with reference to Figure 5, the two tubes 51 and 52, in which there are provided respective ports 53 and 54 with related pressure detectors 55, 56 connected to the differential pressure detector arrangement 10, 10. The respective ports are substantially positioned in the same section of the high-pressure gas supply channel 105 so as to simplify the construction and perturb the regular flow conditions of the blowing gas in saidthe conduit to an even lesser extent.

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A further improved and simplified embodiment of the present invention is shown in Figure 6, in which the two ports 60 and 61 are provided in a same tube 62 extending across saidthe high-pressure gas supply channel 105. These ports must of course be provided in two chambers that are isolated from each other as far as pressure is concerned. For concerned; for this reason, inside said the same tube 62 there is provided a partition wall 63 that isolates from each other the chambers in which saidthe two ports 60 and 61 and the related pressure detectors (not shown). It will of course be appreciated that saidthe partition wall 63 may be assigned various forms and shapes, as shown also in Figure 6A, without affecting the validity and effectiveness of the present invention.

APPARATUS AND METHOD WITH SPECIFICALLY PROVIDED DEVICE FOR AUTOMATIC BURST DETECTION IN BLOW MOULDED CONTAINERS

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ABSTRACT

Apparatus for blow moulding hollow plastic bodies from plastic preforms, or parisons, which is adapted to detect bursts occurring in plastic bottles. To this purpose, the The apparatus itself comprises includes a differential pressure transducer arrangement, a low-pressure gas supply source along with a related first supply channel, a highpressure gas supply source along with a related second supply channel. The differential pressure transducer arrangement is made up by one or more tubes arranged crosswise in the second supply channel. These channel; these tubes contain respective separate chambers opening into the interior of saidthe second supply channel (Pitot tubes). Two sensors adapted to detect respective pressures are connected in a distinct manner to said-the respective chambers. Any possible pressure variation at predetermined moments during the blow-moulding cycle is processed and compared, and the result is an indication of whether a serious irregularity, such as a burst or a silent gas leakage, took place during the blowmoulding process of a given bottle.